

Enhanced transmission through gratings: Structural and geometrical effects

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Abstract

Homogenization theory is used to derive the effective properties of gratings with complex subwavelength structures. Going beyond the effect of the filling fraction, geometrical effects are analyzed using a two step homogenization process. An explicit expression for the transmission spectrum is derived, able to predict the Fabry-Perot resonances and the Brewster angle realizing broadband extraordinary transmission. With the same filling fraction, one expects from this analytical expression that gratings with different geometries may display very different transmission properties. This sensitivity to the microstructure geometry is exemplified in the case of gratings made of hard material and made of dielectric material. The analytical results are shown to be within few percents as compared to full-wave numerical simulations, paving the way for transmission properties tuned by structural and geometrical manipulations.

I. INTRODUCTION

Since the pioneering works of Ebbesen [1], many studies have been conducted on the enhanced transmission through sub-wavelength metallic gratings [2] or sound hard gratings [3] (for a review, see [4]). This extraordinary transmission (EOT in the context of optics and EAT in the context of acoustics) was primarily based on resonances of surface waves (plasmon) and Fabry-Perot resonances, phenomena inherently limited in terms of frequency. More recently, broadband enhanced transmission has been reported [5–8]. This new EOT occurs at an optimal "Brewster" angle corresponding to the impedance matching between the host medium and the metallic grating. Lately, similar enhanced transmission has been reported in the context of acoustic waves for gratings made of impenetrable (sound hard) material [9, 10]. Although some studies have revealed the influence of the grating geometry [11, 12], structural and geometrical effects are in general disregarded. More generally, the gratings are composed by metallic layers for which the controlling parameter is the filling fraction and the attempts to propose simple analytical results were limited to this case [6–10].

In this paper, we consider gratings made of penetrable material, rigid material being a limiting case. We show that the transmission spectra are accurately described by an analytical expression derived after homogenization has been applied, Eq. (4). This expression reveals that the transmission spectra can be strongly affected by geometrical effects, beyond the effect of the filling fraction only. In Section II, the case of single layers is considered. A generalization of the Brewster angle realizing the optimal transmission is obtained and this result is confirmed by comparison with direct numerical calculations. For more complex grating structures, a two step homogenization is applied, leading to expressions of the effective parameters that account for the structural and geometrical characteristics of the grating, Eq. (9). This is done in the Section III. Examples of the geometrical effects on the EOT are presented in Section IV in the non magnetic case (no contrast in B in Eq. (1)) and in the sound hard case. The obtained results are validated by comparison with direct numerical calculations. Technical calculations on the two-step homogenization are collected in the appendix.

II. EXTRAORDINARY TRANSMISSION BY A SINGLE LAYER STRUCTURE

The wave propagation in a grating made of penetrable material can be understood by solving the wave equation in an inhomogeneous medium written in the generic context of acoustic waves

$$\nabla \cdot \left(\frac{1}{\rho(\mathbf{r})} \nabla p(\mathbf{r}) \right) + \frac{\omega^2}{B(\mathbf{r})} p(\mathbf{r}) = 0. \quad (1)$$

Here, the mass density ρ and the bulk modulus B can vary with position \mathbf{r} , allowing contrasts between the host medium (ρ, B) and the grating material (ρ_0, B_0) . Equation (1) can be used with little modification for electromagnetic waves as for shallow water waves.

To begin with, the scattering of a plane wave $p^{(0)}$ at oblique incidence to a grating with single layer structure (SLG) is considered (a time dependence $e^{-i\omega t}$ is understood throughout this paper). The grating has thickness l , with layers of width bd periodically located with d -spacing (Fig. 1). In the low frequency regime, the grating structure can be homogenized

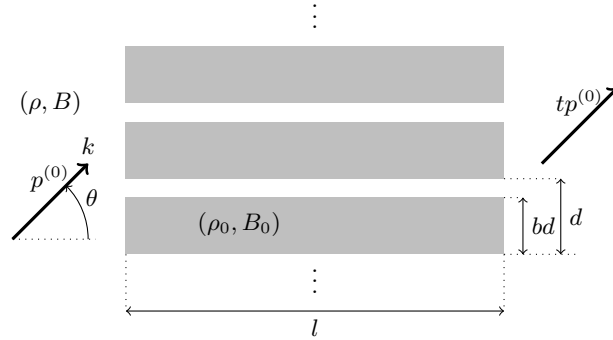


FIG. 1: The geometry of the single layer grating (SLG).

using the homogenization theory of layered media [13], as used to build metamaterials [14]. It results that the grating can be replaced by an homogenized slab. The slab, of length l , is made of an homogeneous anisotropic medium described by the wave equation

$$\nabla \cdot \left[\left(\begin{array}{cc} 1/\rho_{\parallel} & 0 \\ 0 & 1/\rho_{\perp} \end{array} \right) \nabla p \right] + \frac{\omega^2}{B_e} p = 0, \quad (2)$$

with

$$\begin{cases} \frac{1}{\rho_{\parallel}} = \frac{b}{\rho_0} + \frac{(1-b)}{\rho}, \\ \rho_{\perp} = b\rho_0 + (1-b)\rho, \\ \frac{1}{B_e} = \frac{b}{B_0} + \frac{(1-b)}{B}. \end{cases} \quad (3)$$

The transmission coefficient t is

$$t = \frac{4ue^{ikl \cos \theta}}{(1+u)^2 e^{-ik_{\parallel} l} - (1-u)^2 e^{ik_{\parallel} l}}, \quad (4)$$

with

$$u \equiv \frac{k \cos \theta}{k_{\parallel}} \frac{\rho_{\parallel}}{\rho} \quad (5)$$

being the ratio of the effective impedances and where k_{\parallel} is the effective horizontal wavenumber, given by the dispersion relation (from Eq. (2))

$$k_{\parallel}^2 / \rho_{\parallel} + k^2 \sin^2 \theta / \rho_{\perp} = \omega^2 / B_e. \quad (6)$$

The expression of t in Eq. (4) gives the standard Fabry-Perot resonances for $e^{ik_{\parallel} l} = \pm 1$ and the condition of perfect transmission (EOT) when the matched impedance condition is realized: $u = 1$. This homogenization has been already used in the Neumann limit [15] (note also that a non standard homogenization has been proposed in [8], where a more involved dispersion relation is used for k_{\parallel}). The Neumann limit corresponds to $\rho/\rho_0 \rightarrow 0$, $B/B_0 \rightarrow 0$ for which $k_{\parallel} \simeq k$ and $u \simeq \cos \theta / (1 - b)$. Thus, the Fabry-Perot resonances are independent of the incidence angle and the matched impedance condition is obtained at the Brewster angle $\theta = \cos^{-1}(1 - b)$, as reported in experiments performed using grating made of steel [15] or aluminum [10].

Another limiting case corresponds to the case of water waves, or equivalently the case of p-polarized EM wave in a non magnetic dielectric grating. In this case, $B = B_0$ and only the contrast in ρ exists. The figure 2(b) shows the transmission spectrum, $T = |t|^2$, as a function of ρ/ρ_0 and as a function of the incidence angle θ , given by Eq. (4). A validation of this analytical result is done by computing a reference spectrum using full-wave numerical calculations [16]. Results are reported in Figure 2(a): the difference between the two spectra is less than 3% in the whole range of incidence angles and contrasts. The Fabry-Perot resonances appear for certain combinations of $(\rho/\rho_0, \theta)$ that realize $k_{\parallel} l = n\pi$ and, contrary to the Neumann case, these resonances depend on the incidence angle since k_{\parallel} does depend on θ . We have reported in Fig. 2 the optimal angle θ^{opt} realizing the condition of impedance matching, $u = 1$ in Eq. (5) using Eqs. (3) and (6)

$$\theta^{\text{opt}} = \cos^{-1} \sqrt{\frac{(1-b)\rho_0 + b\rho}{\rho_0 + \rho}}, \quad (7)$$

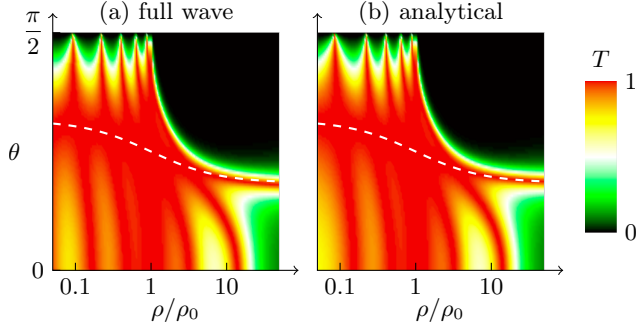


FIG. 2: Transmission spectrum, $T = |t|^2$, as a function of the mass density contrast, ρ/ρ_0 , and of the incidence angle, θ . The grating thickness is $l = 20d$. The layer width is $b = 0.7$ and the frequency is $kd = 0.5$. (a) Full wave calculation, and (b) analytical result Eq. (4). The dashed line indicates the optimal angle, from Eq. (7).

from which the two limits for ρ/ρ_0 can be deduced:

$$\begin{cases} \theta^{\text{opt}}(\rho/\rho_0 \rightarrow 0) = \cos^{-1} \sqrt{1-b}, \\ \theta^{\text{opt}}(\rho/\rho_0 \rightarrow \infty) = \cos^{-1} \sqrt{b}, \end{cases} \quad (8)$$

and these two angles differ from the usual Brewster angle. The perfect transmission is independent of the length l of the grating, as illustrated in Fig. 3, for a small $\rho/\rho_0 = 0.05$ (gratings of lengths $l = 5d$ and $l = d$ are considered). In Fig. 3(a), for a small

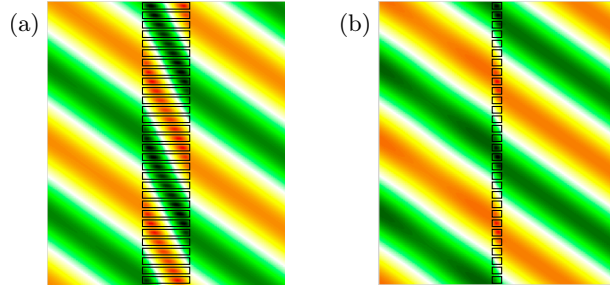


FIG. 3: Spatial distribution of the wave field (real part) at frequency $kd = 1$ in a SLG grating with $b = 0.7$ and for $\rho/\rho_0 = 0.05$, at optimal angle, $\theta^{\text{opt}} \simeq 52.5^\circ$.

ρ/ρ_0 , the wave propagating in the grating resembles the effective wave propagating with $k_{\parallel} \simeq k/(1-b)$, corresponding to a wavenumber inside the structure associated to an angle $\theta^{\text{eff}} = \cos^{-1}[1 + b(1-b)]^{-1/2} < \theta^{\text{opt}}$.

III. THE TWO-STEP HOMOGENIZATION

The robustness of the homogenization for small l values encourages to use further homogenization process for more complex grating structures, as sketched on Fig. 4. Our two step homogenization is inspired from [17] for composite metamaterials. Our "composite" grating is made of a succession of layered structures with two different widths (bd and cd) alternatively stacked next to each other. Each layered structure is first homogenized as previously, resulting in a one dimensional periodic succession of homogeneous anisotropic stacks of respective lengths aL and $(1-a)L$. This latter can be in turn homogenized to form a homogenized anisotropic effective medium, whose effective parameters are

$$\begin{cases} \frac{\rho_{\parallel}}{\rho} = \frac{a}{b\rho/\rho_0 + 1 - b} + \frac{1-a}{c\rho/\rho_0 + 1 - c}, \\ \frac{\rho}{\rho_{\perp}} = \frac{a}{b\rho_0/\rho + 1 - b} + \frac{1-a}{c\rho_0/\rho + 1 - c}, \\ \frac{B}{B_e} = [ab + (1-a)c] \frac{B}{B_0} + [1 - ab - (1-a)c], \end{cases} \quad (9)$$

and the inverse of the effective bulk modulus is simply the average of $1/B$ and $1/B_0$ with the filling fraction $\varphi \equiv [ab + (1-a)c]$ (see Supplementary Material). In the following, we call double layer grating (DLG) the gratings formed by the succession of two layers of different widths b and c , and rectangular inclusion grating (RIG) refers to the particular case $c = 0$.

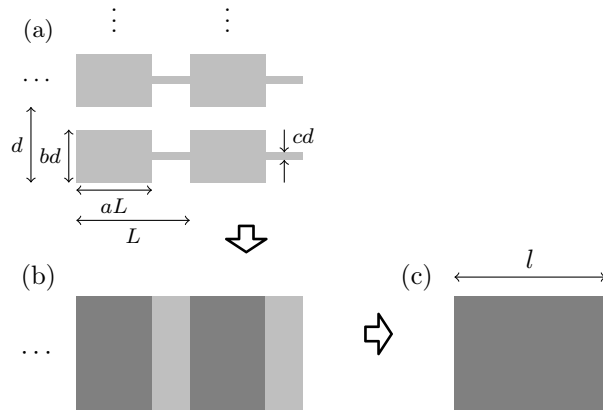


FIG. 4: Two step homogenization. (a) Geometry of the double layer grating (DLG) including the case of rectangular inclusions (RIG) for $c = 0$. (b) The stack composed of two anisotropic layers of respective lengths aL and $(1-a)L$. (c) The resulting homogenized grating of length l .

The expression of the transmission in Eq. (4), with Eqs. (5) and (6), is still valid with

these new expressions of ρ_{\parallel} , ρ_{\perp} and B_e , so that the Fabry-Perot resonances and the optimal angle depend, now, in addition to the value of the contrasts and the filling fraction, on the geometry of the grating. For metallic grating, this geometry has been considered in [11] to enhance the transmission at normal incidence and, in this reference, this was done by decreasing the filling fraction. In fact, inspecting the Neumann limit ($\rho/\rho_0, B/B_0 \rightarrow 0$), one can see that the optimal angle for the SLG is always smaller than for any other structure with the same filling fraction.

IV. GEOMETRICAL EFFECTS ON THE EXTRAORDINARY TRANSMISSION

In the following, we exemplify the effect of the geometry by comparing the transmission spectra of different gratings with the same filling fraction.

First, we consider the limiting case of a rigid material. Fig. 5 shows the transmission spectra of three gratings with different geometries and the same filling fraction $\varphi = 0.4$. The spectra have been calculated using Eq. (4), with Eqs. (5), (6) and (9) and the agreement with full wave numerical computations (not reported) is very satisfactory (within few percents). The influence of the geometry on the spectra is visible, both on the Fabry-Perot resonances and on the impedance matching condition. This is inspected more quantitatively in Fig. 6 where the optimal angle θ^{opt} is plotted as a function of the parameter c . Varying c from 0 to φ , the grating geometry changes from the (RIG) geometry to the simple layer geometry (SLG), experiencing all the geometries of the (DLG) structures with the same filling fraction φ . From Fig. 6, one sees that the optimal angle θ^{opt} can be tuned continuously from about 70° to 52° by increasing c . The case $c = 0$ for which $\theta^{\text{opt}} \simeq 85^\circ$ is a singular limit. Indeed, from Eq. (9), the effective mass density changes from $\rho/\rho_{\perp} = (1 - a)$ for $c = 0$ to $\rho/\rho_{\perp} = 0$ for $c \neq 0$ (with $\rho/\rho_0 \rightarrow 0$).

Next, we consider the case of a non magnetic dielectric material $B = B_0$ (a situation that applies without modification in the context of surface water waves propagating over an uneven bottom). Fig. 7 shows the transmission spectra for a grating with $\rho/\rho_0 = 50$. A remarkable fact is the following: Although the (RIG) and the (DLG) gratings (respectively in Figs. 7(a) and (b)) have very similar geometries, the former grating acts as a low angle pass-filter while the latter behaves as a narrow-band angle filter (around the optimal angle)

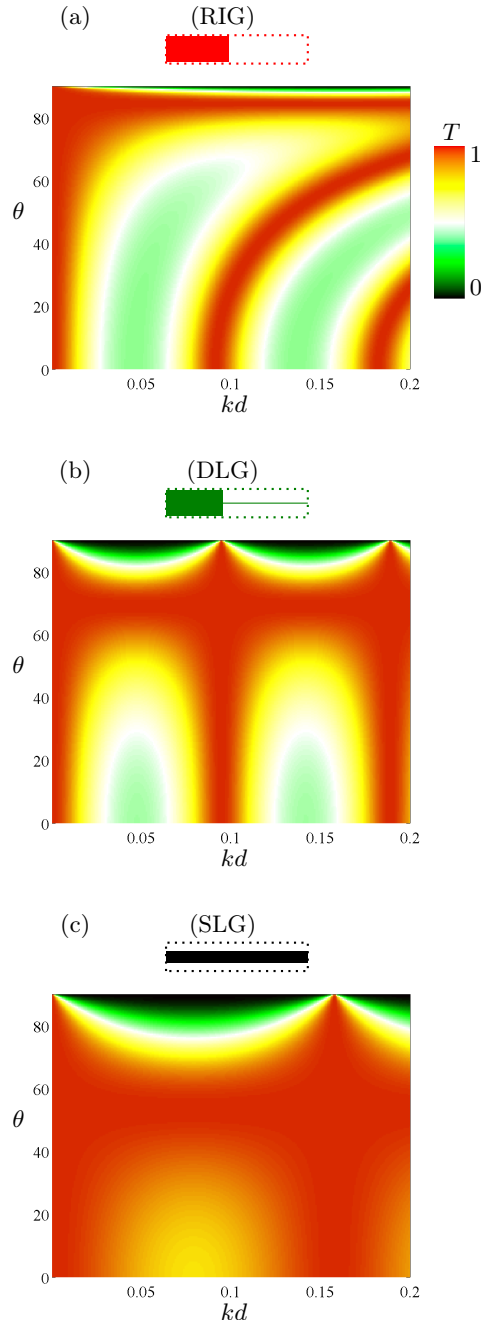


FIG. 5: Transmission spectra of three gratings (rigid material), from Eqs. Eq. (4), with Eqs. (5), (6) and (9). The gratings have the same filling fraction $\varphi = 0.4$ and different geometries. (a) (RIG) with $a = 0.44$ and $b = 0.9$ ($c = 0$), (b) (DLG) with $a = 0.4$, $b = 0.9$ and $c = 0.07$ and (d) (SLG) with $c = \varphi = 0.4$ ($a = 0$). Otherwise $L = 5d$ and $l = 20d$.

and, in both cases, for a wide range of frequencies. The influence of the grating geometry in terms of the parameter c is shown in Fig. 8: varying c produces a change in θ^{opt} from 20° to

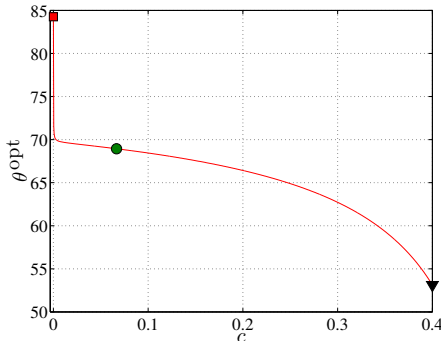


FIG. 6: Influence of the parameter c on the optimal angle θ^{opt} realizing the matching impedance condition $u = 1$. The (DLG) varying c keep the same filling fraction $\varphi = 0.4$, with $b = 0.9$ and $a = (\varphi - c)/(b - c)$. The symbols refer to the gratings considered in Fig. 5, (\square): the (RI) on Fig.5(a), (\circ) the (DLG) on Fig.5(b) and (∇) the (SLG) on Fig.5(c).

50° for the same filling fraction $\varphi = 0.4$. A more subtle effect concerns the occurrence of Fabry Perot resonances. From Eqs. (9) and (6), the effective wavenumber k_{\parallel} is smaller than k and it decreases when c increases (with constant φ and b). Thus, the Fabry-Perot resonances are sent to higher frequencies, resulting in angle filters working for larger frequency ranges.

V. CONCLUSIONS

In summary, homogenization has been shown to be a very efficient tool to analytically predict the transmission spectra of subwavelength gratings with complex geometry. The validity of our prediction has been checked by comparison with full-wave numerical computations. Also, we extended the study to the case of penetrable gratings. This is of interest when considering electromagnetic waves propagating in dielectric material and when considering surface water wave over an uneven bottom. The obtained expression for the transmission spectra allows us to exhibit the geometrical effects, beyond the effect of the filling fraction usually considered. Obviously, the advantage of such analytical results is to be predictive: the description of gratings with variable contrasts and complex geometries involves more and more parameters and using direct numerical computations would be too fastidious to inspect their influences on the transmission.

Our works open a promising way for the design of gratings with transmission properties controlled by structural and geometrical manipulations. Potential applications include di-

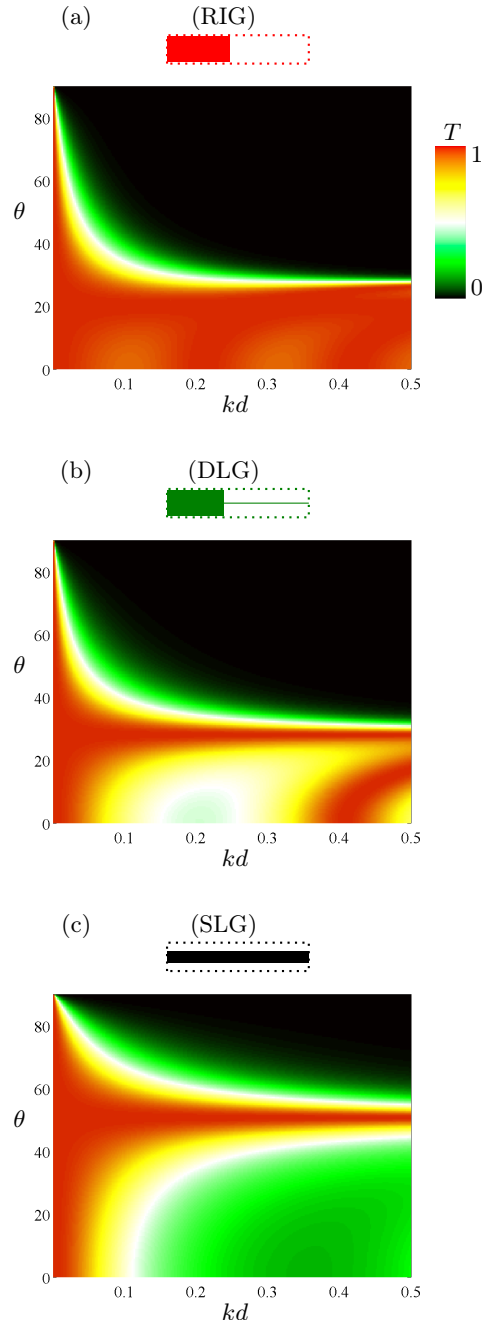


FIG. 7: Same representation as in Fig. 5 for non magnetic material ($B = B_0$) with $\rho/\rho_0 = 50$; the same grating geometries are presented.

rective antenna and directive loudspeakers, antinoise walls, lenses design and water wave focusing.

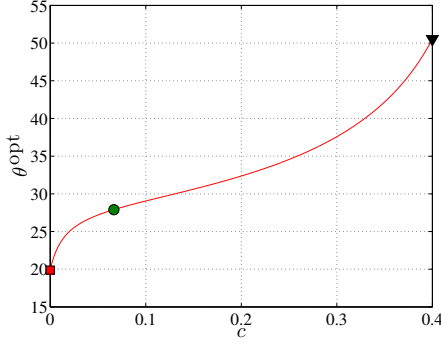


FIG. 8: Same representation as in Fig. 6 for the three gratings of Fig. 7.

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Appendix A: The two step homogenization

We report the main steps leading to Eq. (9). To do that, we first use classical homogenization of layered medium (1) with horizontal layers (Fig. 1). We get, for layers of filling fraction b

$$\nabla \cdot \left[\begin{pmatrix} 1/\rho_{\parallel}^{(b)} & 0 \\ 0 & 1/\rho_{\perp}^{(b)} \end{pmatrix} \nabla p \right] + \frac{\omega^2}{B_e^{(b)}} p = 0, \quad (\text{A1})$$

and we use, for ρ and B depending on the vertical direction (say y) $1/\rho_{\parallel}^{(b)} = \langle 1/\rho(y) \rangle$, $\rho_{\perp}^{(b)} = \langle \rho(y) \rangle$ and $1/B_e^{(b)} = \langle 1/B_e(y) \rangle$, where $\langle f(y) \rangle \equiv (1/d) \int_0^d dy f(y)$ denotes the spatial average.

$$\begin{cases} \frac{1}{\rho_{\parallel}^{(b)}} = \frac{b}{\rho_0} + \frac{(1-b)}{\rho}, \\ \rho_{\perp}^{(b)} = b\rho_0 + (1-b)\rho, \\ \frac{1}{B_e^{(b)}} = \frac{b}{B_0} + \frac{(1-b)}{B}. \end{cases} \quad (\text{A2})$$

The same result applies for a medium (2) made of horizontal layers of filling fractions c and the resulting effective parameters are $\rho_{\parallel}^{(c)}$, $\rho_{\perp}^{(c)}$ and $B_e^{(c)}$. The DLG structure consists in a succession of vertical layers of medium (1) and medium (2), as shown on Fig. 4(b). This DLG structure can be homogenized, considering the filling fraction a for the medium (1) (and $(1-a)$ for the medium (b)). The structure has now effective parameters varying along

the horizontal direction (say x), so that the homogenization of the layered structure is such that $\rho_{\parallel} = \langle \rho_{\parallel}(x) \rangle$, $1/\rho_{\perp} = \langle 1/\rho_{\perp}(x) \rangle$ and $1/B_e = \langle 1/B_e(x) \rangle$.

We get a resulting homogenized anisotropic structure (as in Eq. (3)), with

$$\begin{cases} \rho_{\parallel} = a\rho_{\parallel}^{(b)} + (1-a)\rho_{\parallel}^{(c)}, \\ \frac{1}{\rho_{\perp}} = \frac{a}{\rho_{\perp}^{(b)}} + \frac{(1-a)}{\rho_{\perp}^{(c)}}, \\ \frac{1}{B_e} = \frac{a}{B_e^{(b)}} + \frac{(1-a)}{B_e^{(c)}}, \end{cases} \quad (\text{A3})$$

leading to the expressions in Eq. (9).

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